

The AM noise mechanism in oscillators

Enrico Rubiola and Rémi Brendel

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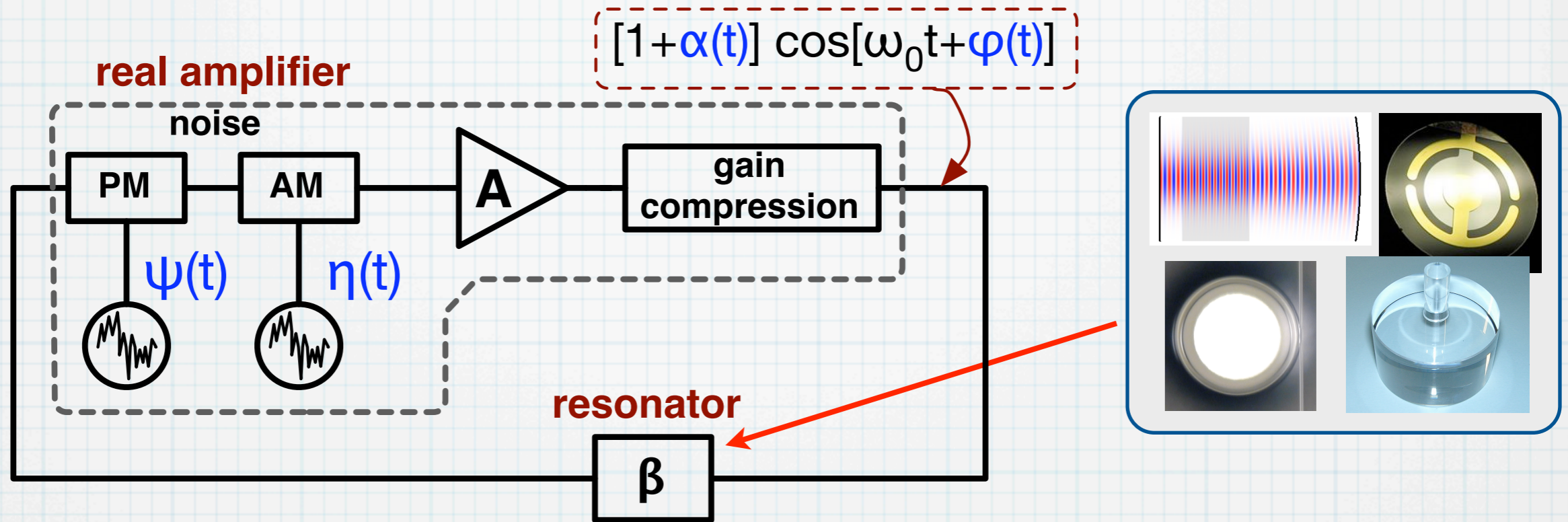
Outline

- Introduction
- low-pass representation of the oscillator
- Generalization of the Leeson effect
- Analytical solutions and simulations

$$[1 + \alpha(t)] \cos[\omega_0 t + \varphi(t)]$$

home page <http://rubiola.org>

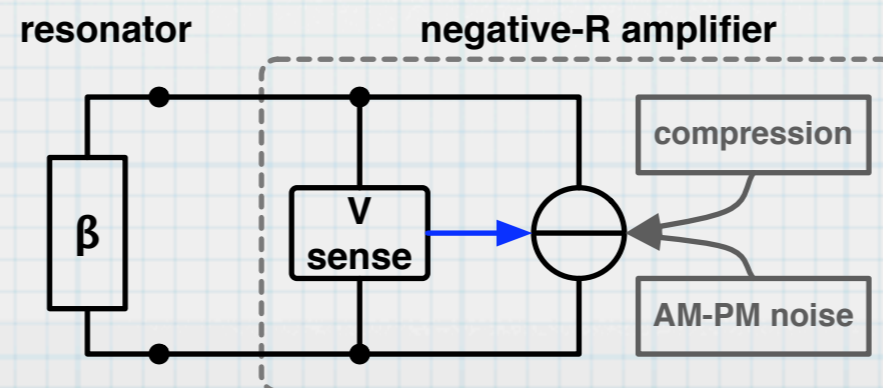
General oscillator model



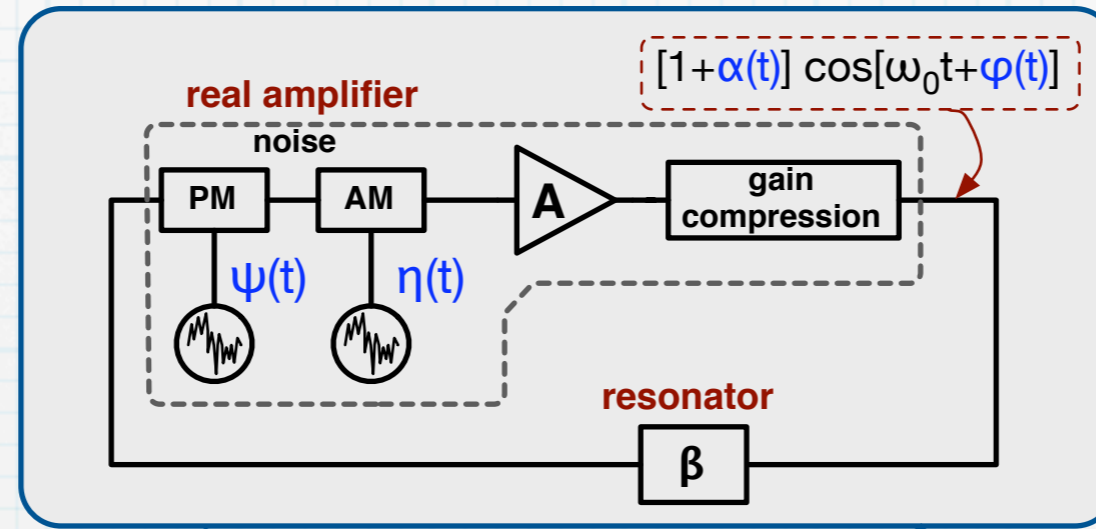
Barkhausen condition $A\beta = 1$ at ω_0

Let A fluctuate $\Rightarrow A \rightarrow (1 + \eta) \exp(j\psi)$

The model also describes the negative-R oscillator

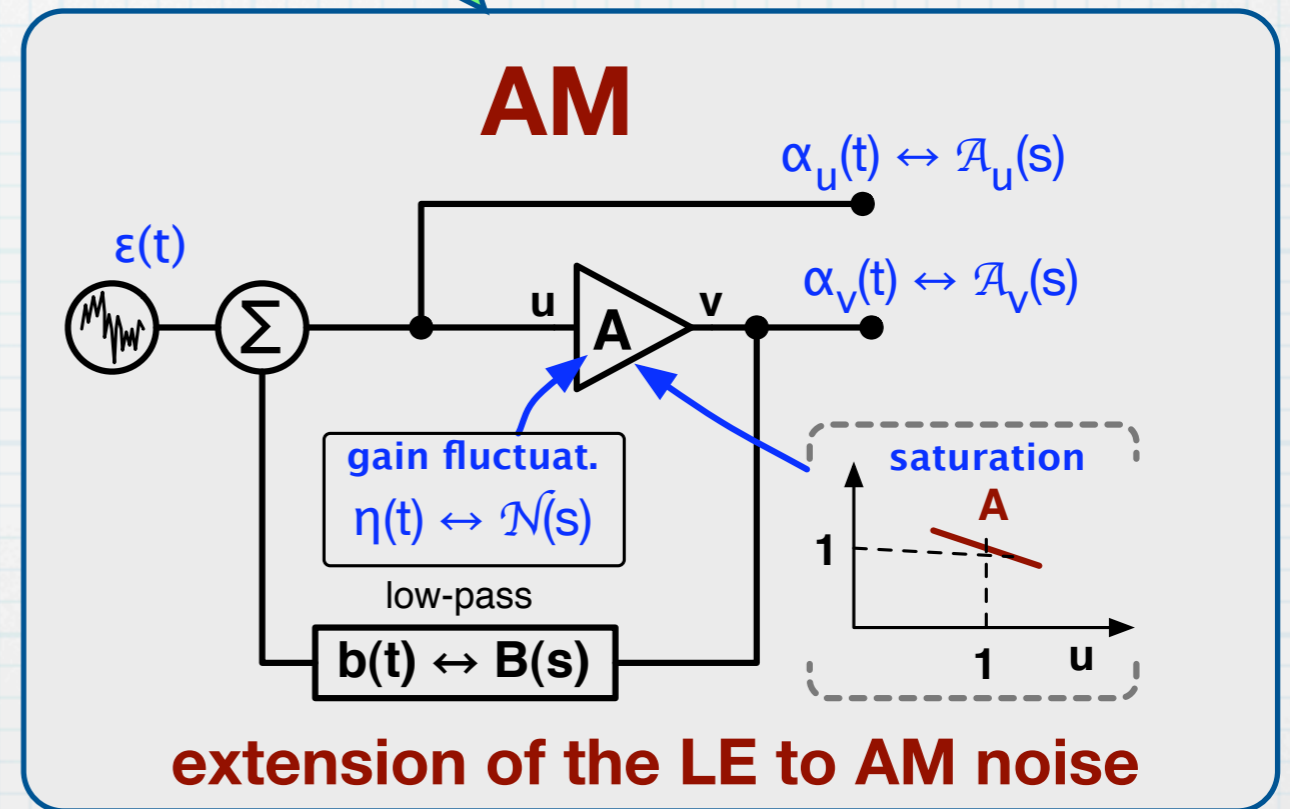
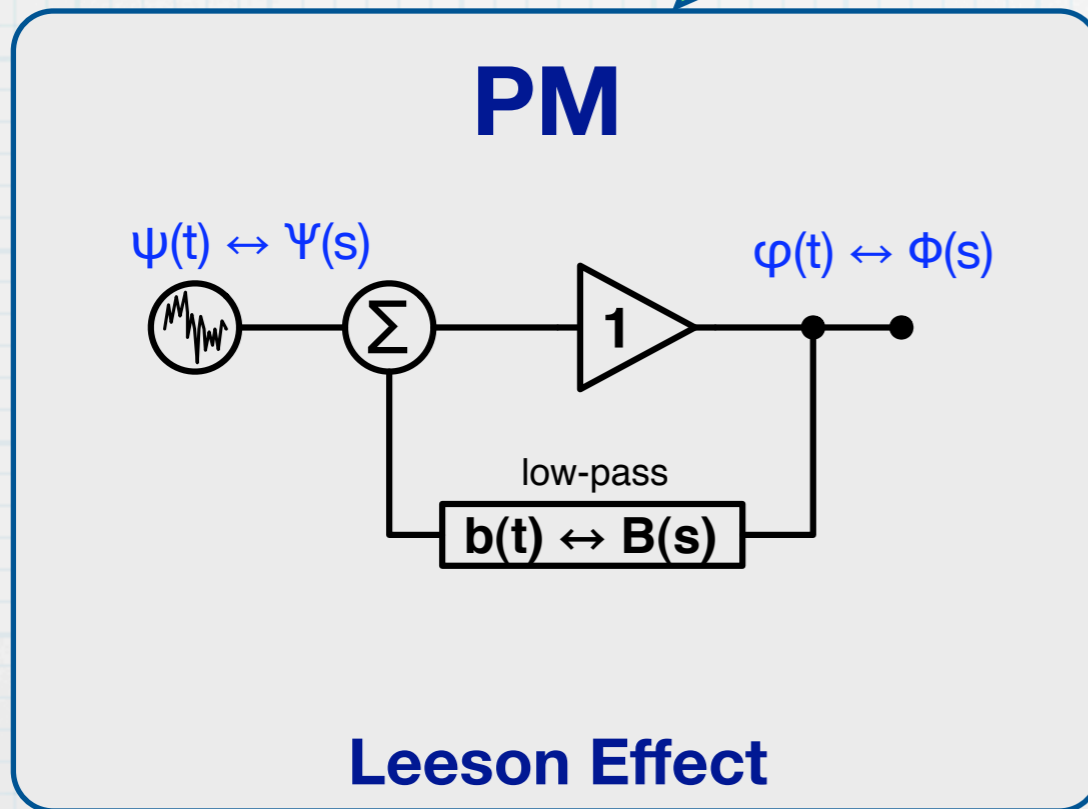


Low-pass representation of AM-PM noise



RF, μ waves
or optics

low-pass equivalent



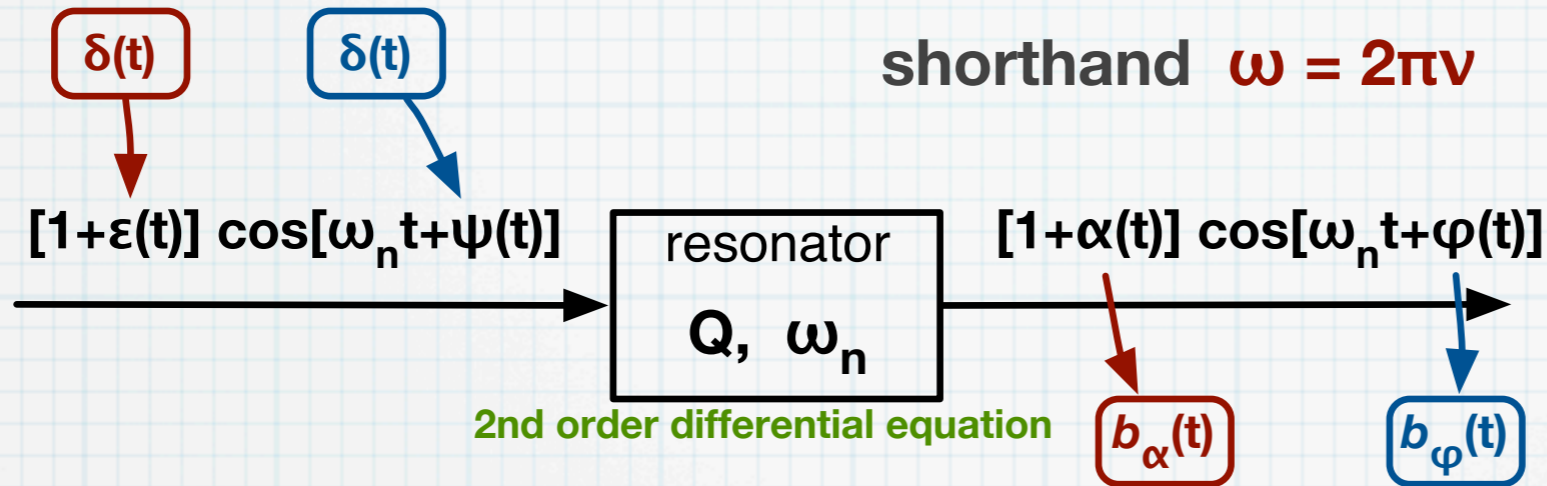
The amplifier

- “copies” the input phase to the out
- adds phase noise

The amplifier

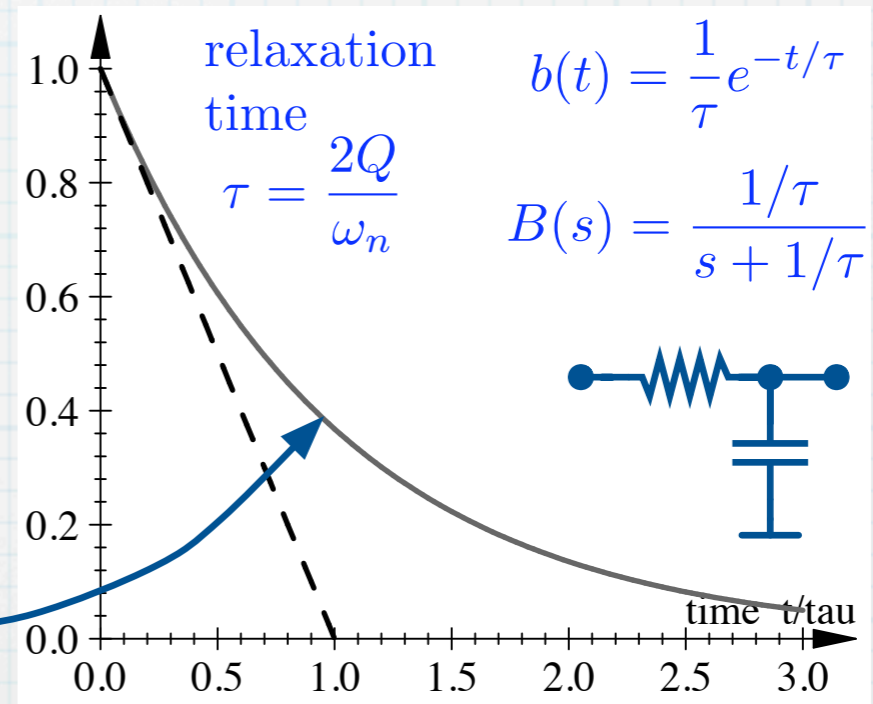
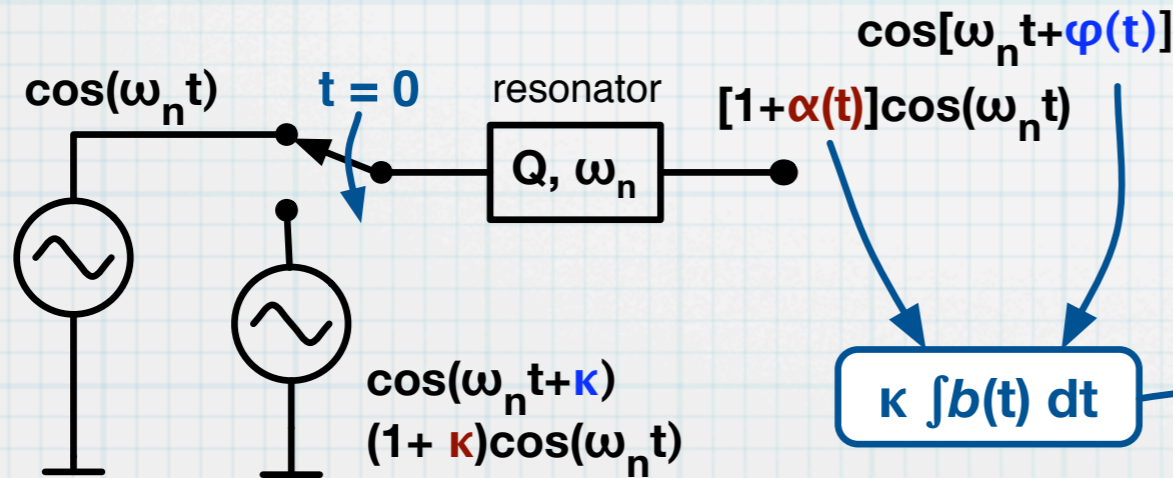
- compresses the amplitude
- adds amplitude noise

Resonator impulse response



$\omega_n = \omega_0$
 $\omega_n =$ natural frequency
 $\omega_0 =$ oscillation frequency

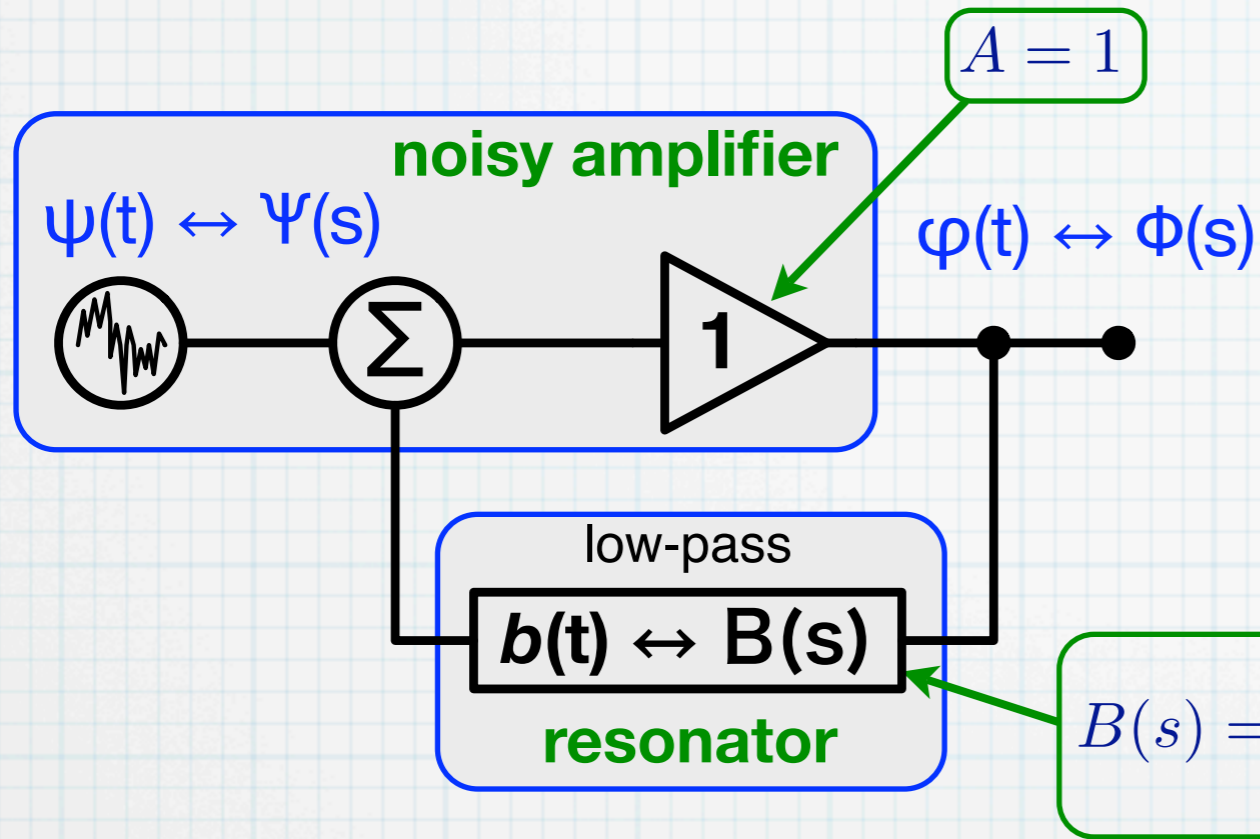
set a small phase or amplitude step κ at $t=0$, and linearize for $\kappa \rightarrow 0$



— boring mathematics omitted —

The low-pass equivalent of a resonator is a 1st order low-pass filter
The time constant is equal to the resonator relaxation time τ

Leeson effect

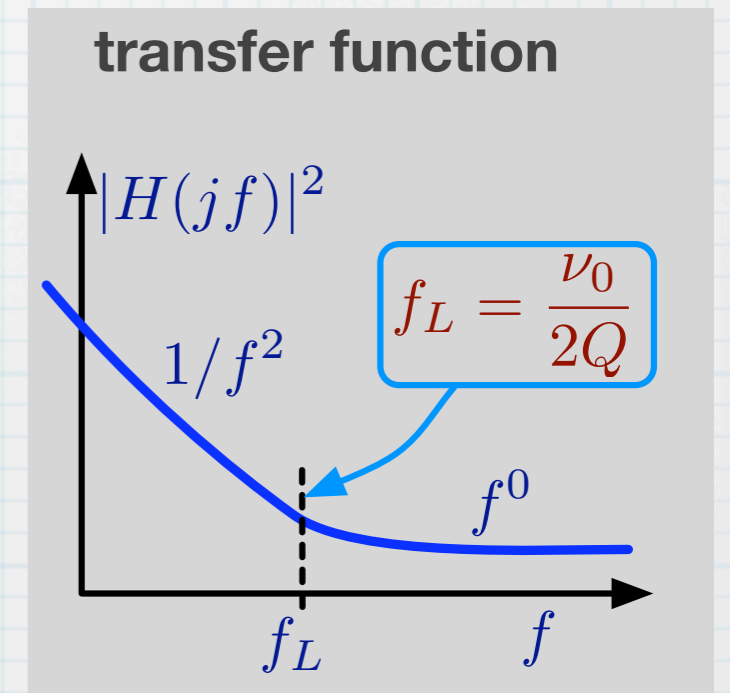
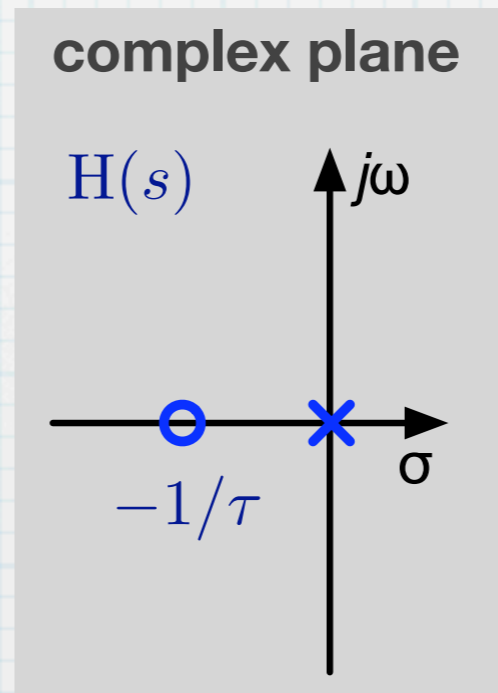
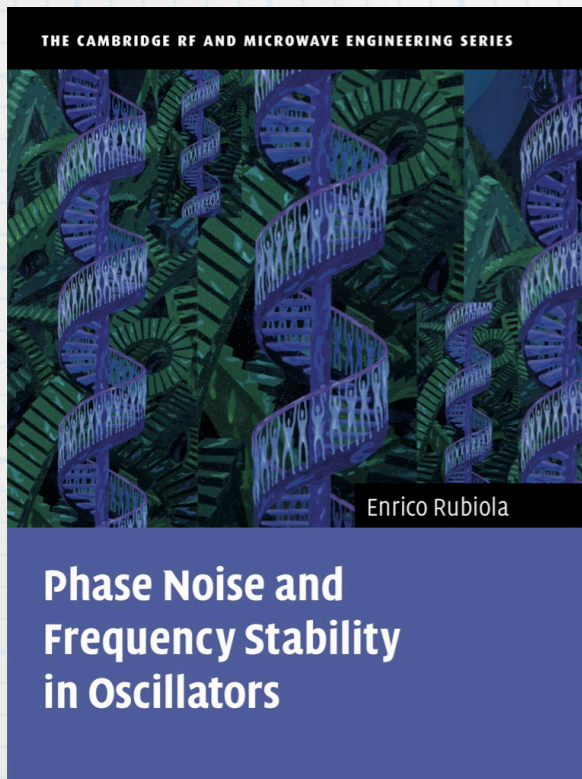


phase-noise transfer function

$$H(s) = \frac{\Phi(s)}{\Psi(s)} \quad \text{definition}$$

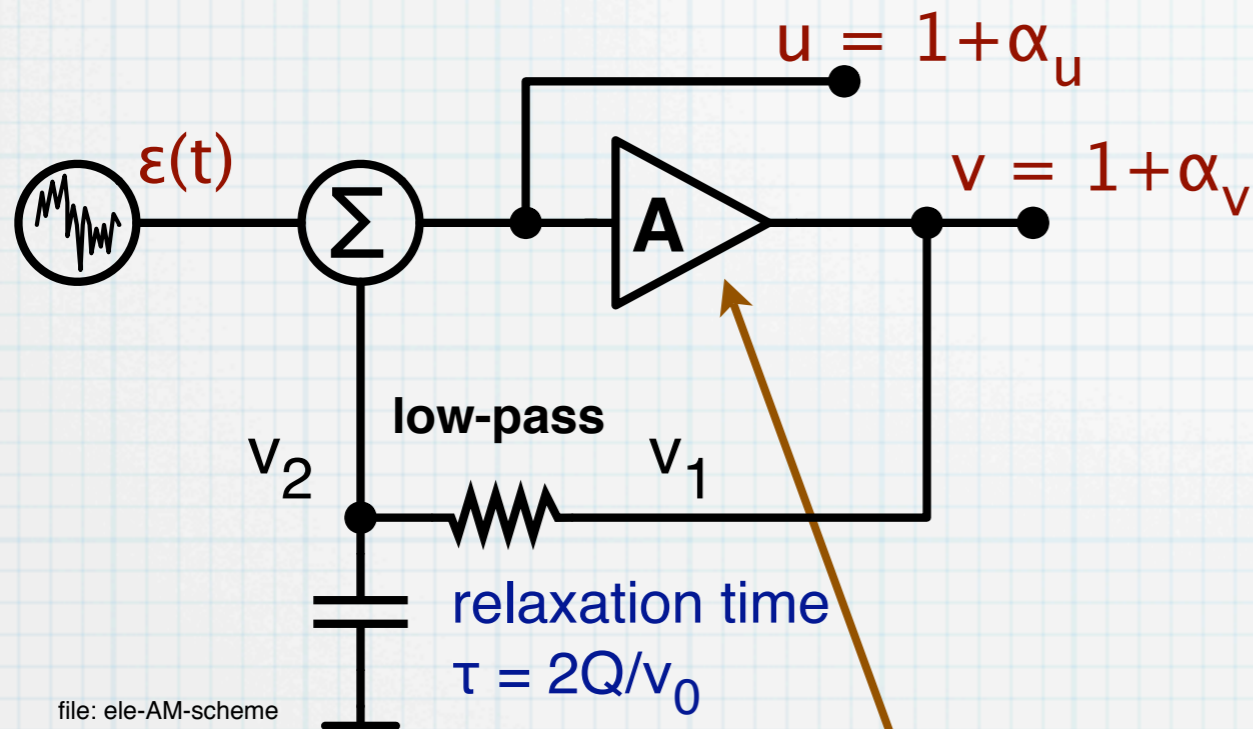
$$H(s) = \frac{1}{1 + AB(s)} \quad \text{general feedback theory}$$

$$H(s) = \frac{1 + s\tau}{s\tau} \quad \text{Leeson effect}$$



Low-pass model of amplitude (1)

First we need to relate the system restoring time τ_r to the relaxation time τ



simple feedback theory

$$u = \epsilon + v_2$$

$$v_2 = \frac{1}{\tau} \int (v_1 - v_2) dt$$

$$v_1 = v = Au$$

$$v_2 = u - \epsilon$$

$$u = \epsilon + \frac{1}{\tau} \int (A - 1)u + \epsilon dt$$

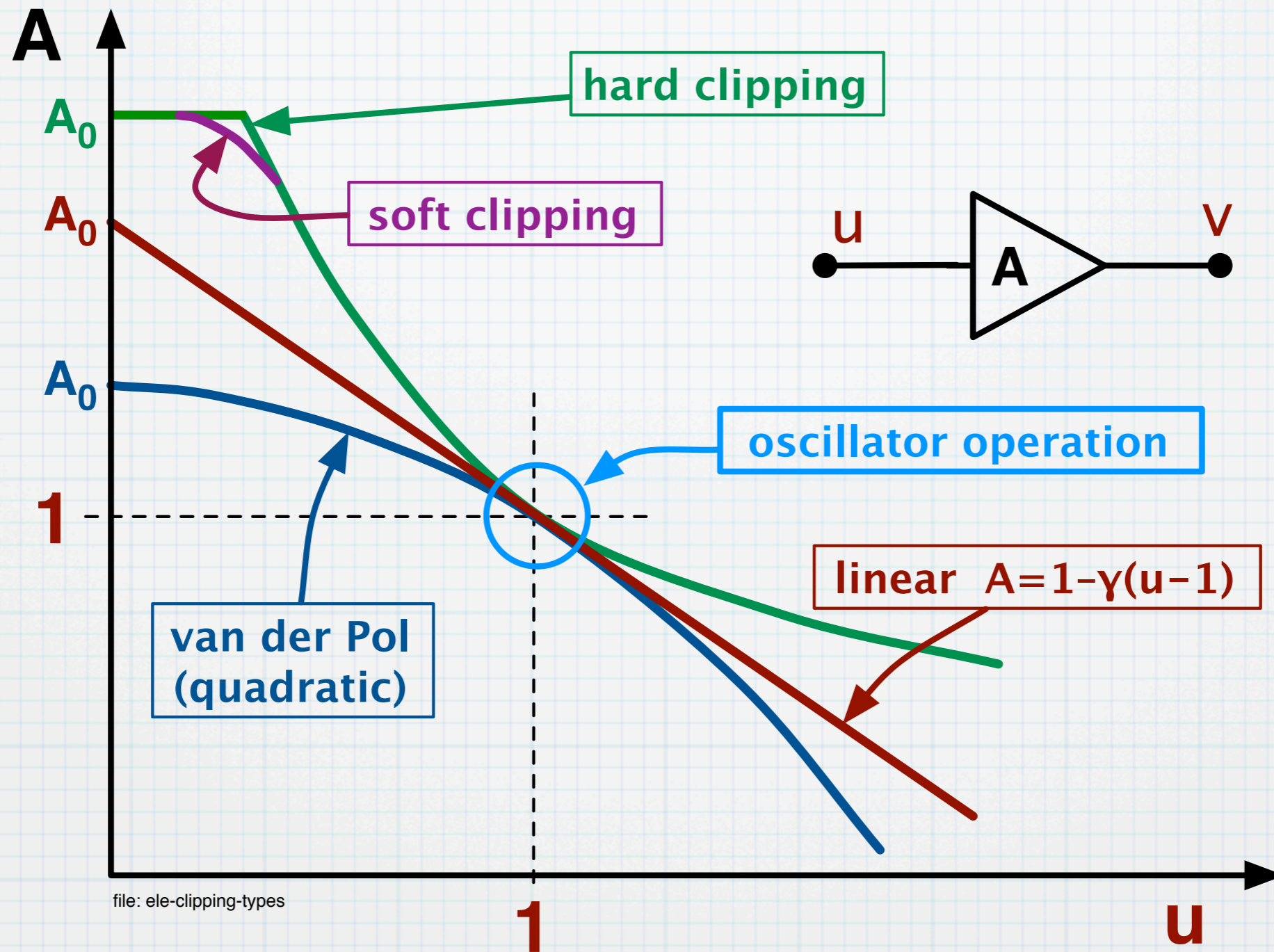
differential equation

$$\dot{u} - \frac{1}{\tau} (A - 1) u = \frac{1}{\tau} \epsilon + \dot{\epsilon}$$

Gain compression is necessary for the oscillation amplitude to be stable

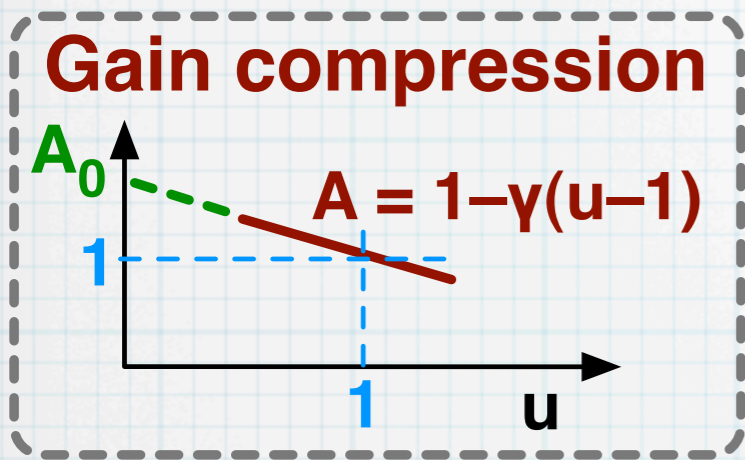
The Laplace / Heaviside formalism cannot be used because the amplifier is non-linear

Common types of gain saturation



Gain compression is necessary for the oscillation amplitude to be stable

Low-pass model of amplitude (2)

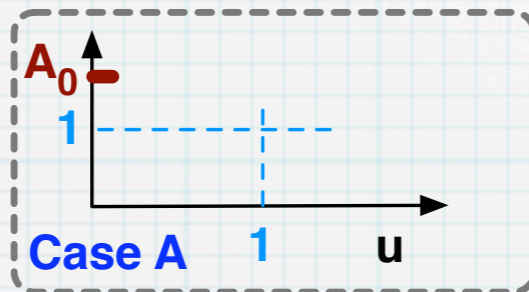


homogeneous
differential
equation

$$\dot{u} - \frac{1}{\tau} (A - 1) u = 0$$

Three asymptotic cases

At low RF amplitude, let the gain be an arbitrary value denoted with A_0

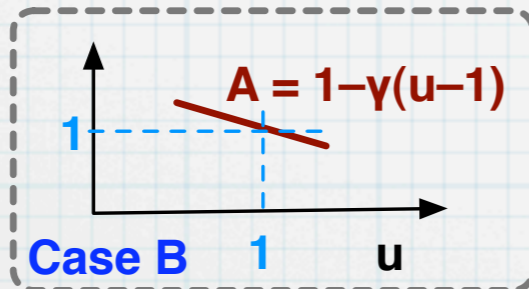


Startup: $u \rightarrow 0$, $A \rightarrow A_0 > 1$

$$\dot{u} - \frac{1}{\tau} (A_0 - 1) u = 0 \Rightarrow u = C_1 e^{(A_0 - 1) t / \tau}$$

rising exponential

For small fluctuation of the stationary RF amplitude, the gain varies linearly with V

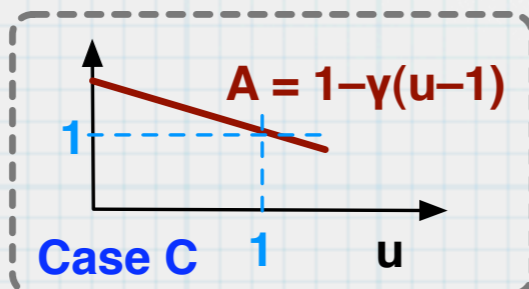


Regime: $u \rightarrow 1$, $A = 1 - \gamma(u-1)$

$$\dot{u} + \frac{\gamma}{\tau} (u-1) u = 0 \Rightarrow u = C_2 e^{-\gamma t / \tau}$$

restoring time constant $\tau_r = \tau / \gamma$

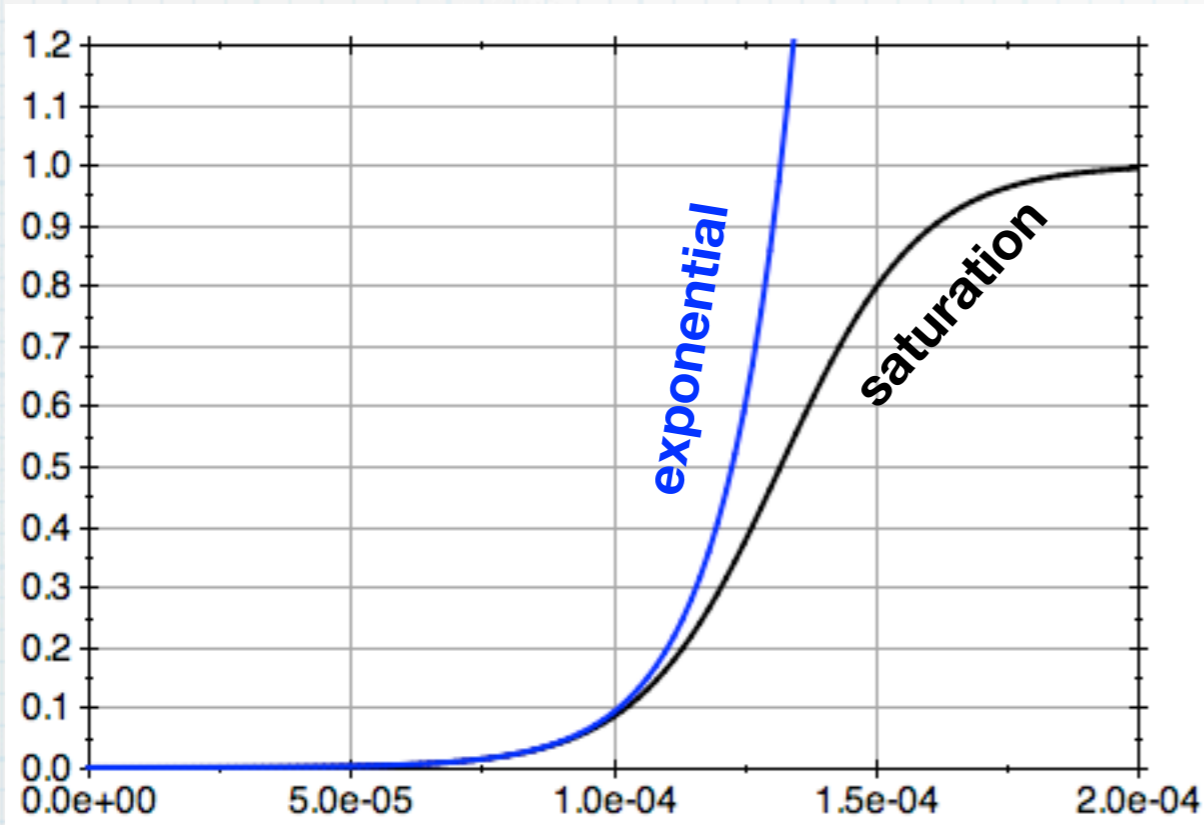
Simplification: the gain varies linearly with V in all the input range



Linear gain: $A = 1 - \gamma(u-1)$

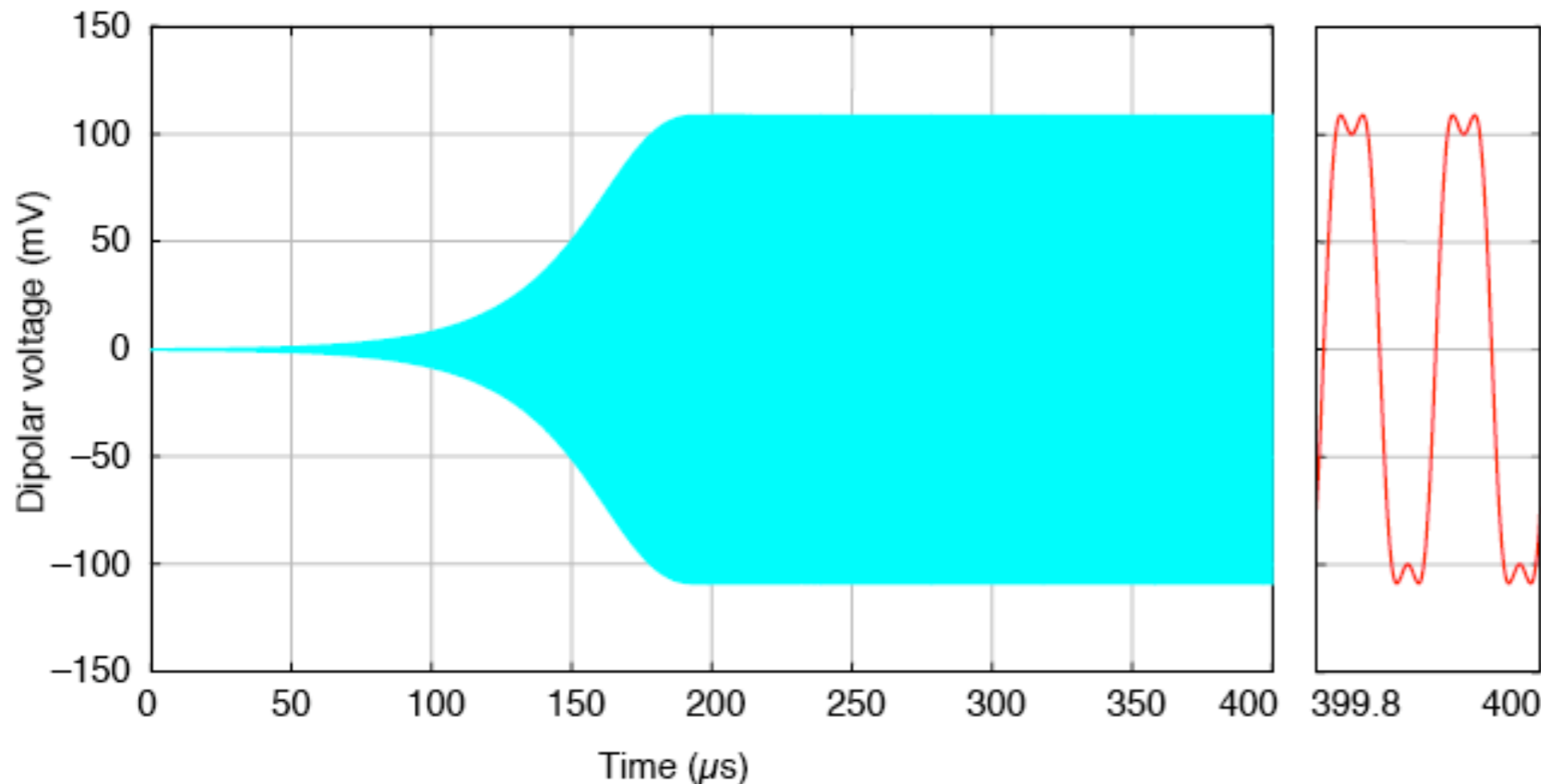
$$u = \frac{1}{\left(\frac{1}{u(0)} - 1\right) e^{-\gamma t / \tau} + 1}$$

Startup – analysis vs. simulation



analytical solution,
 $A = 1 - \gamma(u-1)$

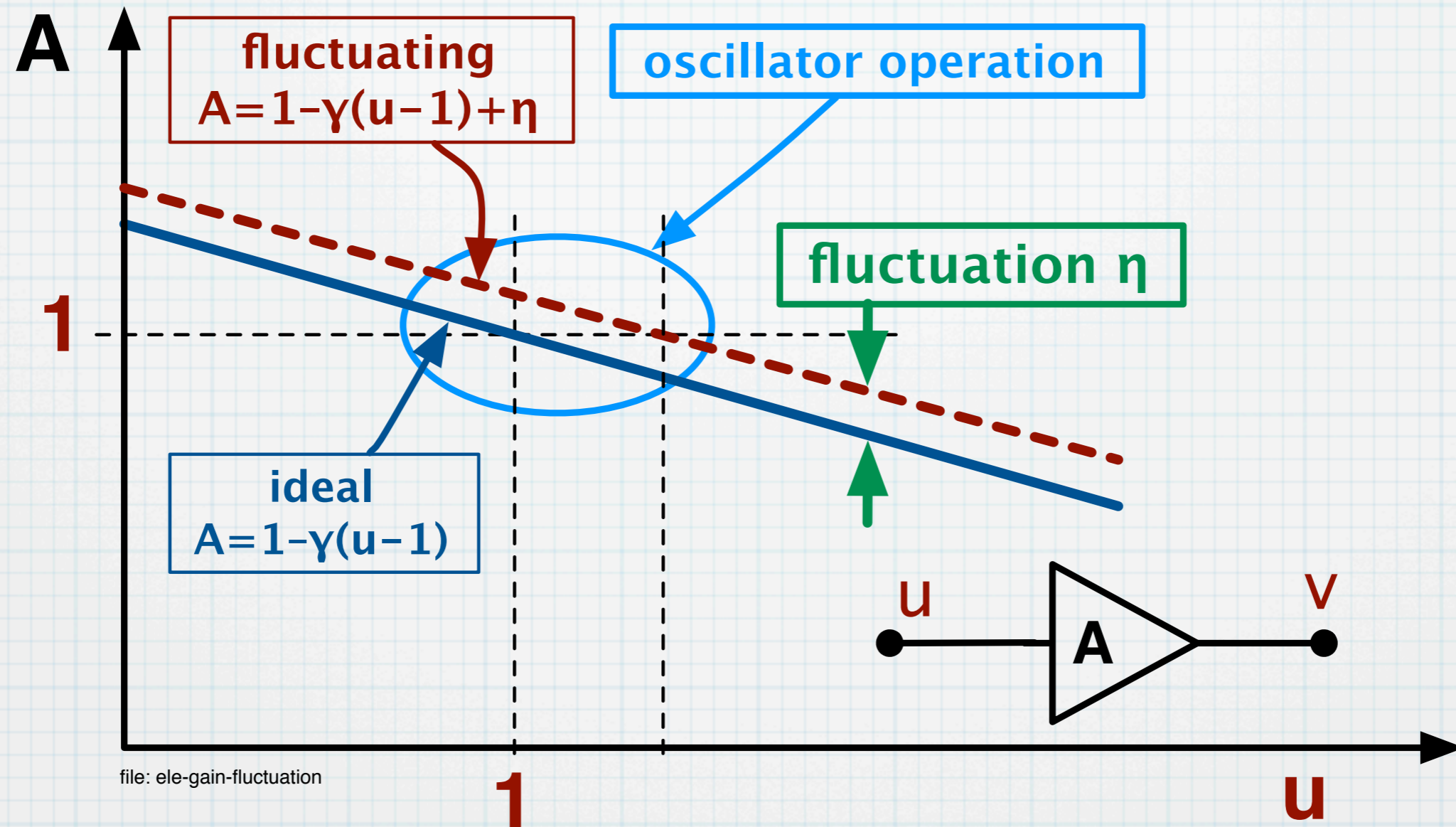
10 MHz oscillator
L = 1 mH
R = 125 Ω
Q ~ 503



van der Pol oscillator
 simulated by RB

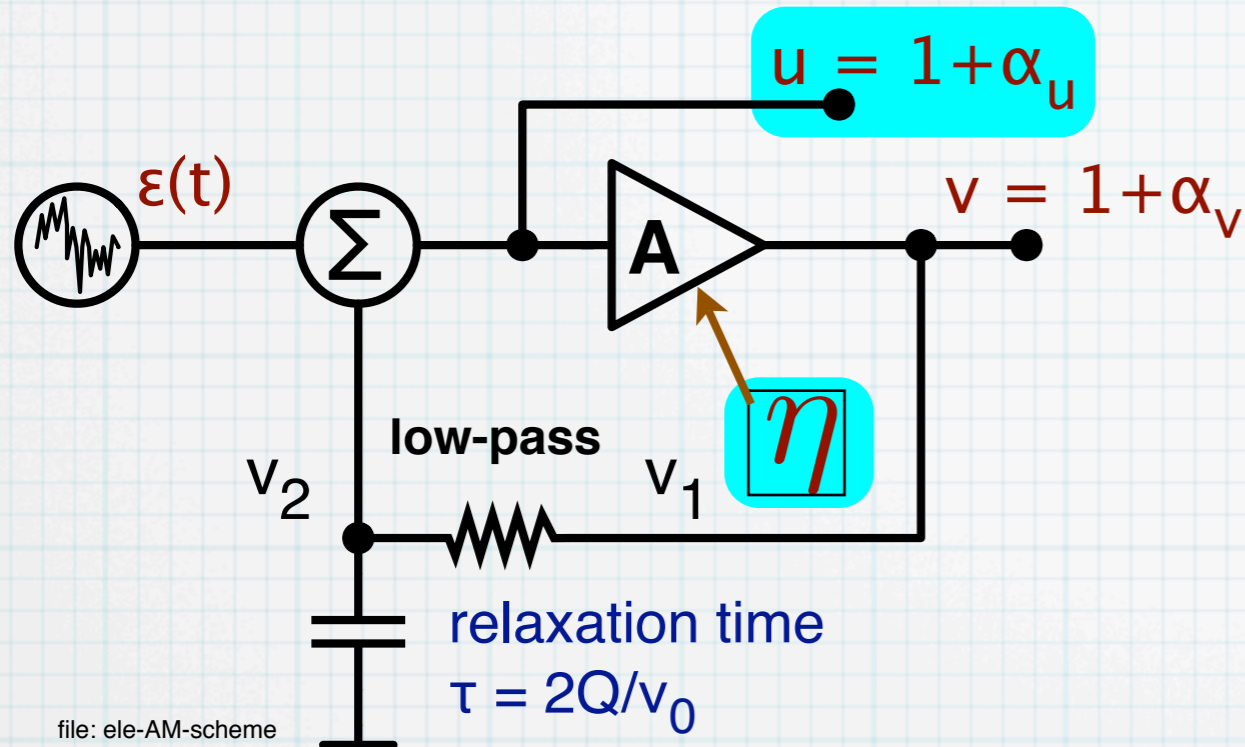
Rising exponential.
We find the same
time constant $-\tau/\gamma$

Gain fluctuations – definition



Gain compression is necessary for the oscillation amplitude to be stable

Gain fluctuations – output is u



$$\dot{u} = \frac{1}{\tau} (A - 1)u \quad \text{non-linear equation}$$

$$A = 1 - \gamma(u - 1) + \eta$$

$$\dot{u} + \frac{\gamma}{\tau} (u - 1)u = \frac{\eta}{\tau} u \quad \text{linearization for low noise}$$

\downarrow \downarrow \downarrow \downarrow \downarrow
 $\dot{\alpha}_u$ α_u 1 1

$$\dot{\alpha}_u + \frac{\gamma}{\tau} \alpha_u = \frac{1}{\tau} \eta \quad \text{linearized equation}$$

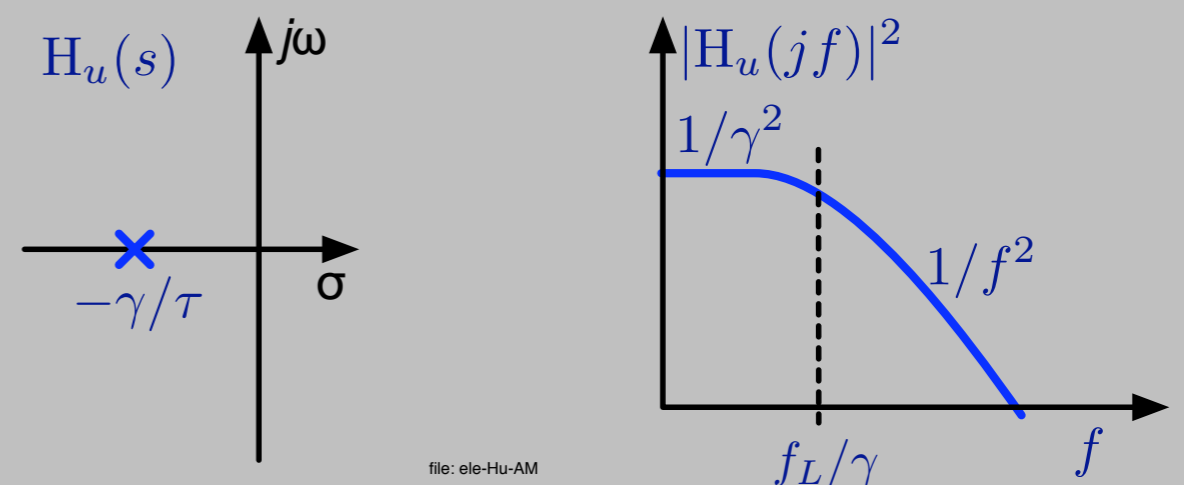
$$\left(s + \frac{\gamma}{\tau}\right) \mathcal{A}_u(s) = \frac{1}{\tau} \mathcal{N}(s) \quad \text{Laplace transform}$$

Linearize for low noise and use the Laplace transforms

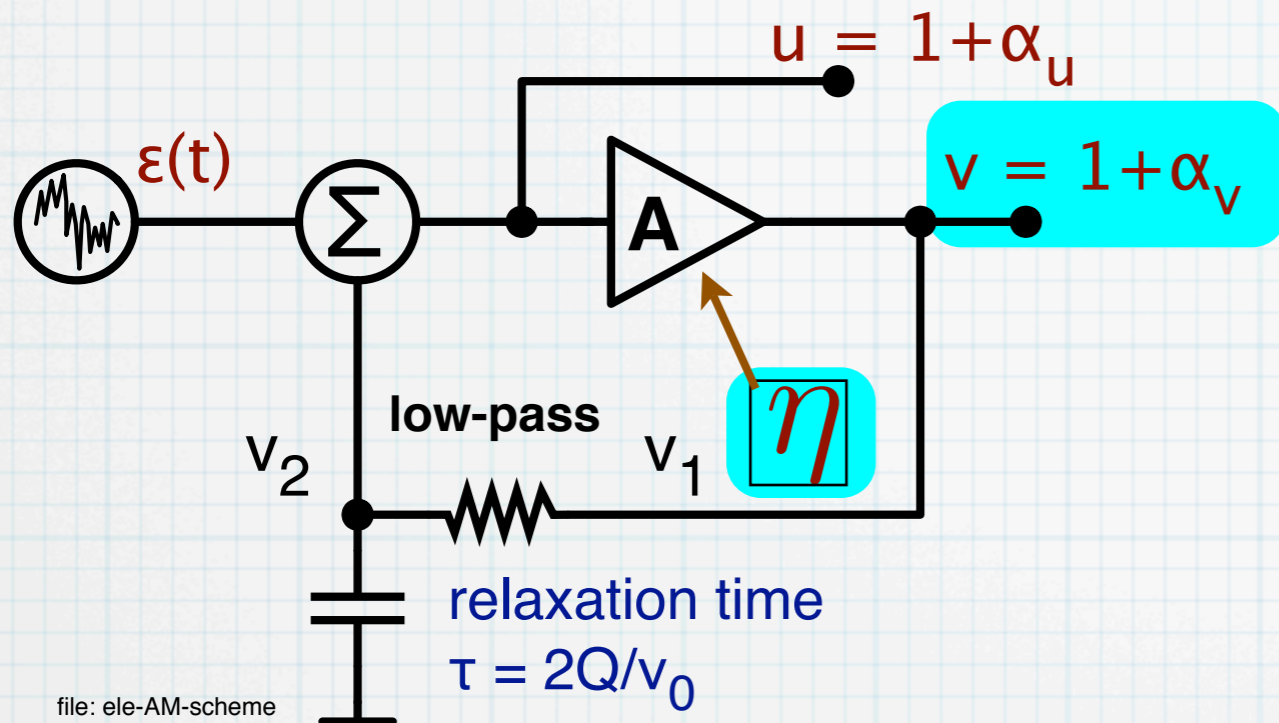
$$\alpha_u(t) \leftrightarrow \mathcal{A}_u(s) \quad \text{and} \quad \eta(t) \leftrightarrow \mathcal{N}(s)$$

$$H_u(s) = \frac{\mathcal{A}_u(s)}{\mathcal{N}(s)} \quad \text{definition}$$

$$H_u(s) = \frac{1/\tau}{s + \gamma/\tau} \quad \text{result}$$



Gain fluctuations – output is v



$$\left(s + \frac{\gamma}{\tau}\right) \mathcal{A}_u(s) = \frac{1}{\tau} \mathcal{N}(s) \quad \text{starting equation}$$

$$\mathcal{A}_u(s) = \frac{\mathcal{A}_v(s) - \mathcal{N}(s)}{1 - \gamma}$$

$$\left(s + \frac{\gamma}{\tau}\right) \mathcal{A}_v(s) = \left(s + \frac{1}{\tau}\right) \mathcal{N}(s)$$

$$H(s) = \frac{\mathcal{A}_v(s)}{\mathcal{N}(s)} \quad \text{definition}$$

$$H(s) = \frac{s + 1/\tau}{s + \gamma/\tau} \quad \text{result}$$

boring algebra relates α_v to α_u

$$v = Au$$

$$A = -\gamma(u - 1) + 1 + \eta$$

$$v = [-\gamma(u - 1) + 1 + \eta] u$$

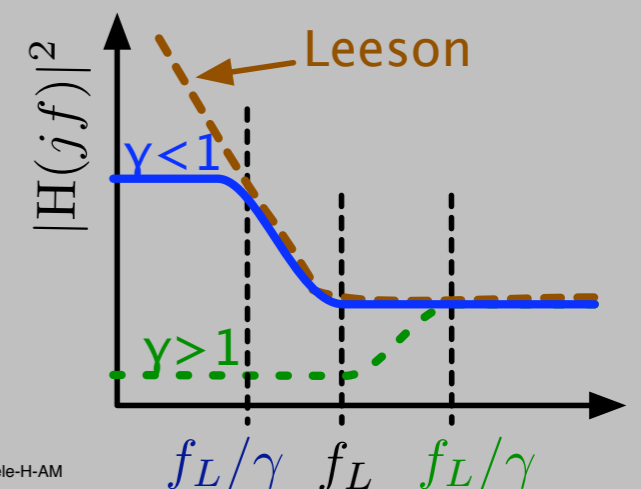
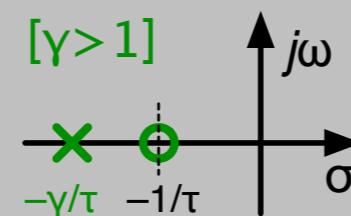
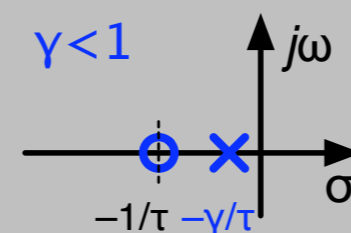
$$v = [-\gamma\alpha_u + 1 + \eta] [1 + \alpha_u]$$

$$\cancel{1} + \alpha_v = \cancel{1} + \eta - \gamma\alpha_u + \alpha_u - \alpha_u\eta - \gamma\alpha_u^2$$

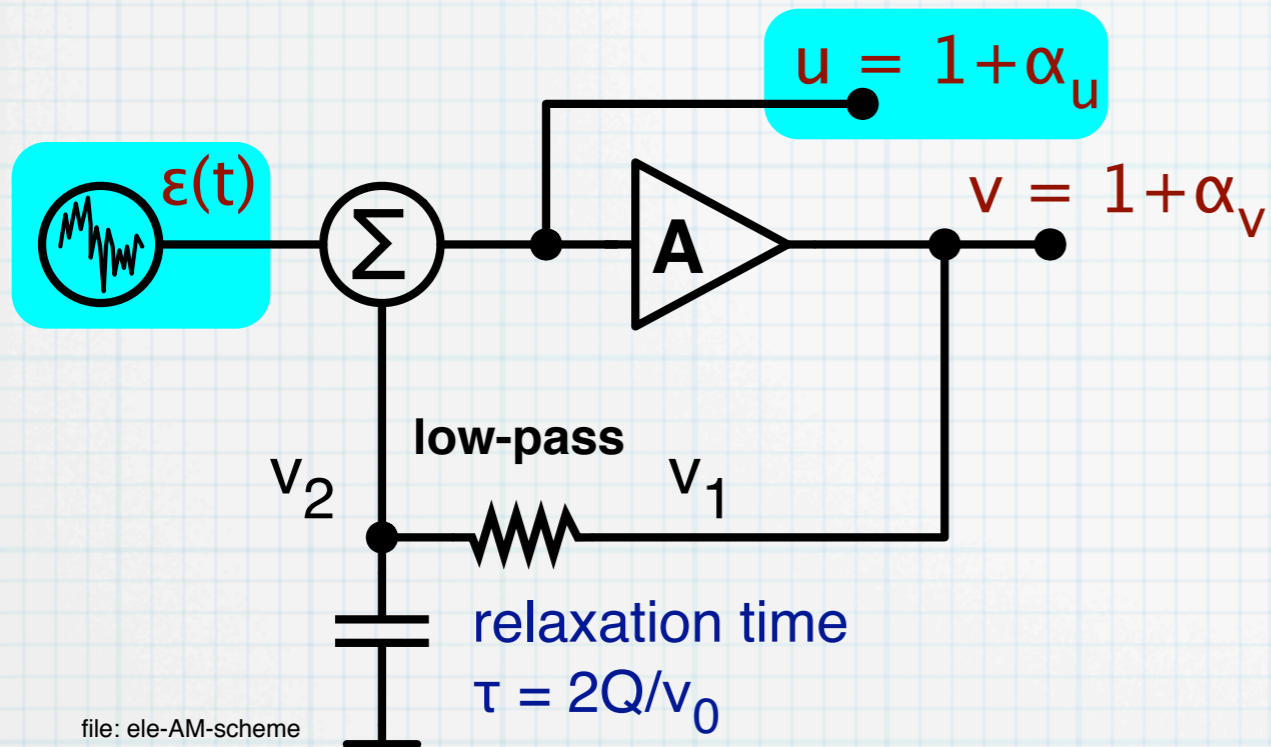
$$\alpha_v = (1 - \gamma)\alpha_u + \eta$$

$$\alpha_u = \frac{\alpha_v - \eta}{1 - \gamma}$$

linearization
for low noise



Additive noise – output is u



$$\dot{u} = \frac{1}{\tau} (A - 1)u + \dot{\epsilon} + \frac{1}{\tau} \epsilon \quad \text{non-linear equation}$$

$A = 1 - \gamma(u - 1)$

$$\dot{u} + \frac{\gamma}{\tau} (u - 1)u = \dot{\epsilon} + \frac{1}{\tau} \epsilon \quad \text{lineariz. for low noise}$$

$\dot{\alpha}_u \quad \alpha_u \quad 1$

$$\dot{\alpha}_u + \frac{\gamma}{\tau} \alpha_u = \dot{\epsilon} + \frac{1}{\tau} \epsilon \quad \text{linearized equation}$$

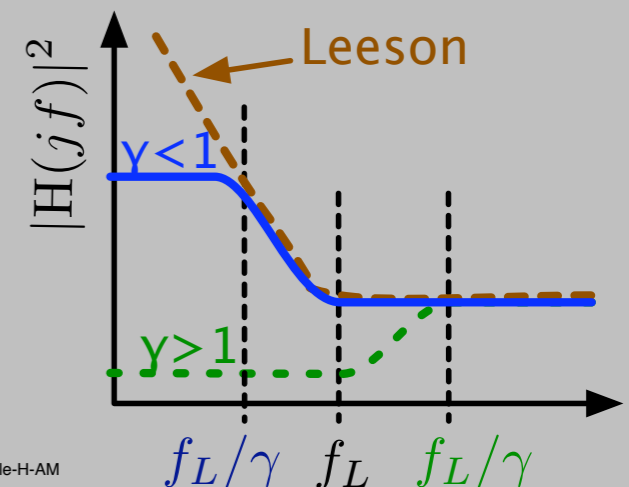
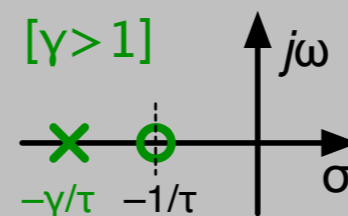
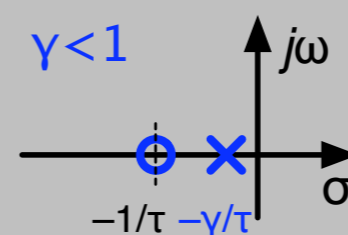
$$\left(s + \frac{\gamma}{\tau}\right) \mathcal{A}_u(s) = \left(s + \frac{1}{\tau}\right) \mathcal{E}(s) \quad \text{Laplace transform}$$

Linearize for low noise and use the Laplace transforms

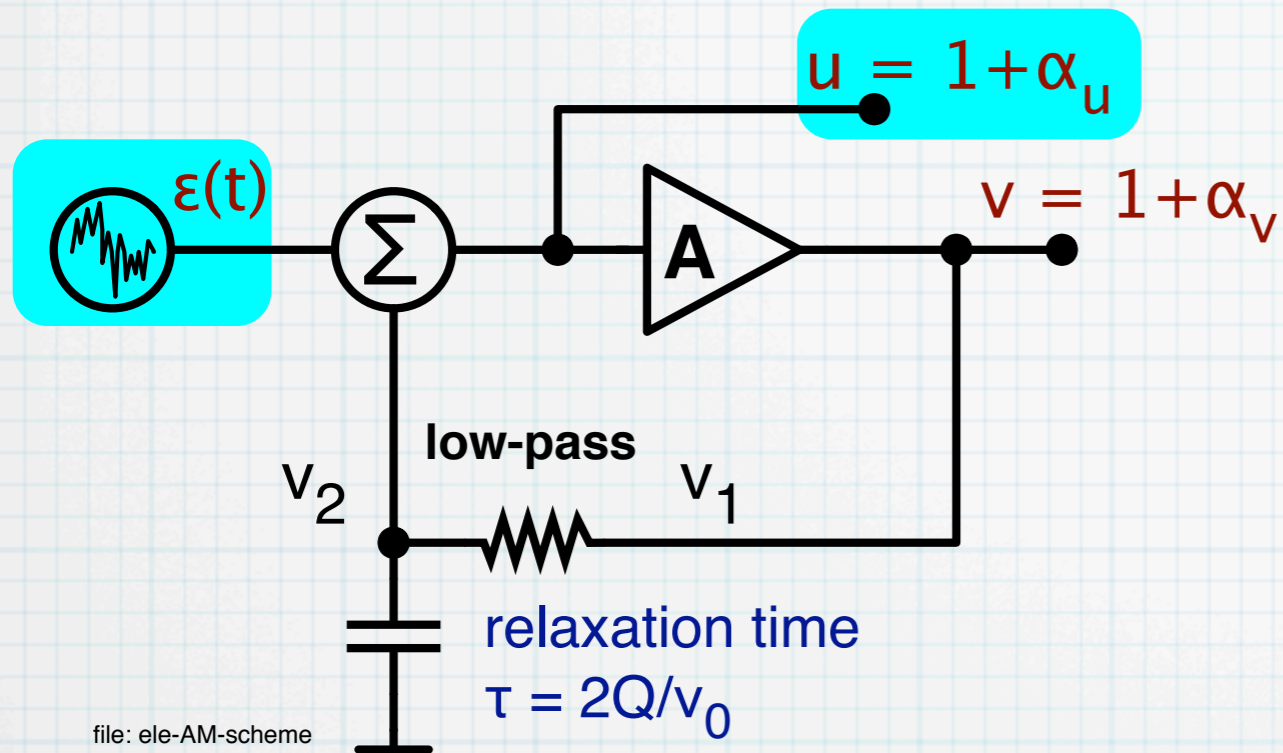
$$\alpha_u(t) \leftrightarrow \mathcal{A}_u(s) \quad \text{and} \quad \epsilon(t) \leftrightarrow \mathcal{E}(s)$$

$$H_u(s) = \frac{\mathcal{A}_u(s)}{\mathcal{E}(s)} \quad \text{definition}$$

$$H_u(s) = \frac{s + 1/\tau}{s + \gamma/\tau} \quad \text{result}$$



Additive noise – output is v



boring algebra relates α' to α

$$v = Au$$

$$A = 1 - \gamma(u - 1)$$

$$v = [1 - \gamma(u - 1)]u$$

$$1 + \alpha_v = [1 - \gamma\alpha_u][1 + \alpha_u]$$

$$\cancel{1} + \alpha_v = \cancel{1} + \alpha_u - \gamma\alpha_u - \gamma\alpha_u^2$$

$$\alpha_v = (1 - \gamma)\alpha_u$$

$$\alpha_u = \frac{\alpha_v}{1 - \gamma}$$

linearization
for low noise

$$\dot{\alpha}_u + \frac{\gamma}{\tau}\alpha_u = \dot{\epsilon} + \frac{1}{\tau}\epsilon$$

$$\alpha_u = \alpha_v / (1 - \gamma)$$

linearized
equation

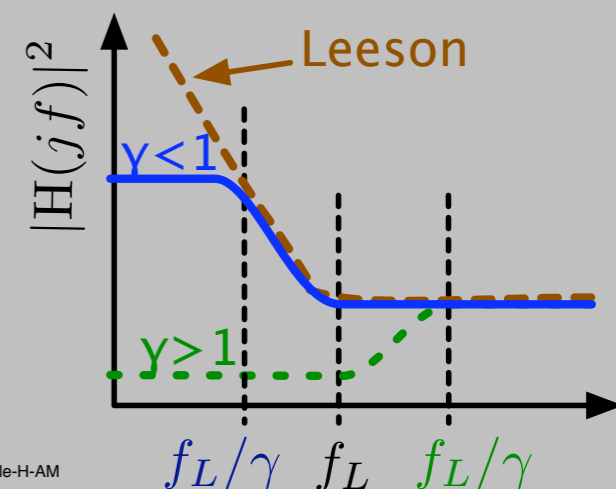
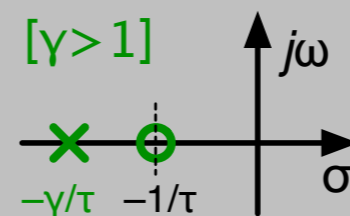
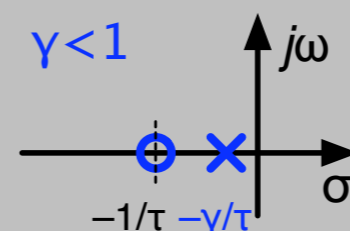
$$\frac{1}{1 - \gamma} \left(\dot{\alpha}_v + \frac{\gamma}{\tau}\alpha_v \right) = \dot{\epsilon} + \frac{1}{\tau}\epsilon$$

$$\frac{1}{1 - \gamma} \left(s + \frac{\gamma}{\tau} \right) \mathcal{A}_v(s) = \left(s + \frac{1}{\tau} \right) \mathcal{E}(s) \quad \text{Laplace transform}$$

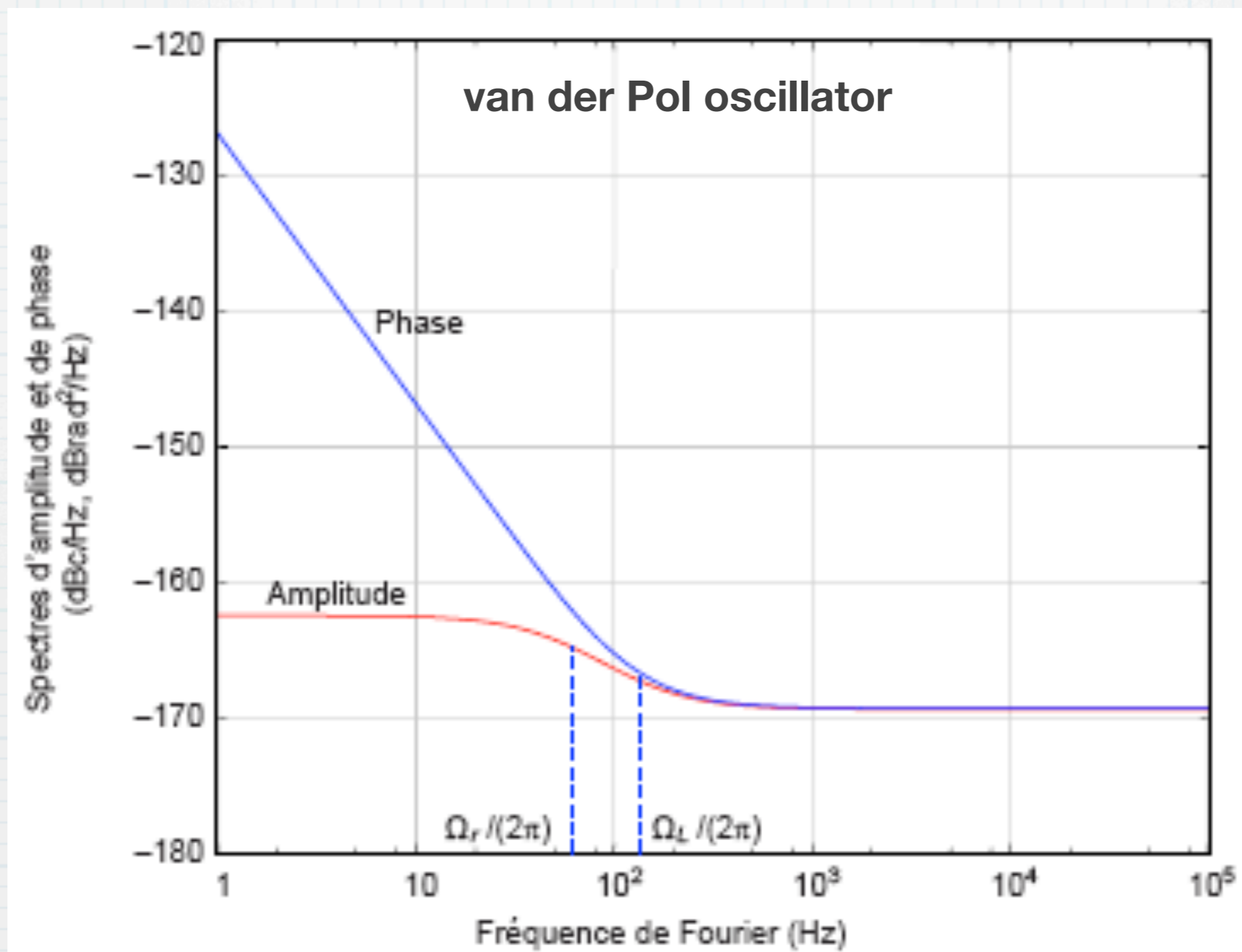
$$H(s) = \frac{\mathcal{A}_v(s)}{\mathcal{E}(s)}$$

definition

$$H(s) = (1 - \gamma) \frac{s + 1/\tau}{s + \gamma/\tau} \quad \text{result}$$



Simulation (RB)



Analytic model and numeric simulation
yield same time constants and slopes

Conclusions

- **Well-established framework, fully tested with PM noise**
- **Extension of the Leeson effect to the oscillator AM noise**
- **Simple analytical model and theory**
- **The analytical model (ER) is in agreement with the simulations (RB), developed independently**
- More emphasis is given to the analytical model *only* because
 - final formulae are easier to implement
 - the talk is given by ER
- **AM-FM coupling via Miller effect**
(notice that other types of coupling exist)
- **Experiments starting soon. The sapphire oscillator gives easy access to (almost) all parameters**